

Wireless Power Transmission Through Air, Wood & Concrete Medium At Utility Frequency Of 50hz

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Abstract – An attempt is made to perform wireless power transmission using circuits resonating at the utility frequency of 50 Hz. The purpose of this project is to develop a method for transmitting electrical power through air, wood and concrete walls. An equation for the theoretical transmission efficiency that considers the copper and core losses was derived through equivalent circuit analysis. There is good agreement between the experimental and calculated values. The transmission efficiency was found to be strongly dependent on the shape of the magnet pole pieces. The ultimate goal of the present project is, simulation is done using mat lab and hardware design is done and obtained values are compared with theoretical and simulated values. There are three possible methods of wireless power transmission (WPT) electromagnetic induction, magnetic resonance, and radio waves. In the present study, the efficiency of resonant power transmission through concrete was investigated at the utility frequency of 50 Hz, using magnet pole piece configurations.

Index terms: wood, concrete, frequency, magnetic resonance, wireless power transmission (WPT).



1 INTRODUCTION

The ultimate goal of the present project is to develop a method for transmitting a power operating in structures that humans cannot enter, such as areas contaminated by radioactivity, which is an issue that has become increasingly urgent in the wake of the Fukushima nuclear disaster. This would require energy being sent through thick concrete walls, possibly containing steel frames, so that workers could avoid contamination.

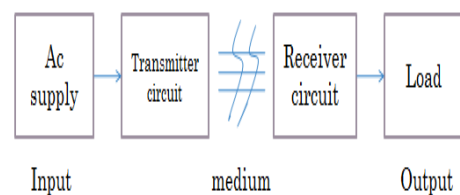
Thus there is a desire to use wireless power technology to eliminate the remaining wired power connection. Presently, several wireless power techniques are being pursued. The idea of wireless power transfer originates from the inconvenience of having too many wires sharing a limited amount of power sockets. We believe that many people have the same experience of lacking enough sockets for their electronic devices. Wireless Power Transfer via Strongly Coupled Magnetic Resonances by André Kurs, Aristeidis Karalis, Robert Moffatt, J. D. Joannopoulos, Peter Fisher, Marin Soljacic. Using self-resonant coils in a strongly coupled regime, we experimentally demonstrated efficient non-radioactive power transfer over distances up to 8 times the radius of the coils. We were able to transfer 60 watts with 40% efficiency over distances in excess of 2 meters. We present a quantitative model describing the power transfer, which matches the experimental results to within 5%. We discuss the practical applicability of this system and suggest directions for further study. Wireless Power

Transmission through Concrete Using Circuits Resonating at Utility Frequency of 60Hz by Hiroki Ishida and Hiroto Furukawa

IEEE the efficiency of resonant power transmission through concrete was investigated at the utility frequency of 60 Hz, using three different magnet pole piece configurations. The effect of a steel frame embedded in the concrete was also evaluated.

In the present research paper, the efficiency of resonant power transmission through air, wood and concrete is calculated at the utility frequency of 50Hz using mat lab programming, for magnetic pole piece configurations. Mat lab simulation is also done.

2 BLOCK DIAGRAM



- A. Source: AC supply given here is.
- B. Transmitter coil: The transmitter coil is the one which transmits power wirelessly to the receiver coil.
- C. Receiver coil: The receiver coil is the one which receives power from the transmitter coil.
- D. Load 100watt incandescent bulb

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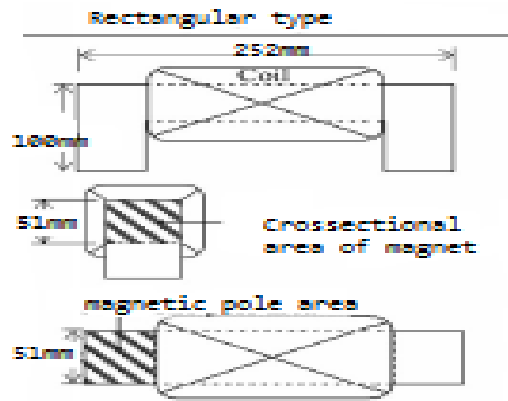


Fig.(2):- WPT system: (a) circuit diagram and (b) Equivalent circuit.

At a frequency of 60 Hz, no saturation of the pole pieces was observed up to a flux density of 0.7 T. The coils were wound from single-strand enamel covered copper wire with a diameter of 1.42 mm. These prototypes were designed based on an assumed operating voltage and current of 200 V 5A to 10 A, respectively. The same type of coil was used for the transmitter and receiver circuits. We predicted the transmission power efficiency through analysis of the equivalent circuit of a 60-Hz WPT system. The parameters of the equivalent circuit used in the calculation (i.e., the transformer constants) were determined experimentally using an actual WPT device.

3 CIRCUIT ANALYSIS

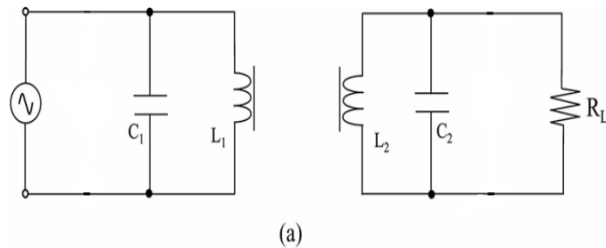


Fig. 2(a) shows a circuit diagram of the WPT system. The secondary condenser C_2 was connected in parallel with the load (PP mode). The configuration with C_2 connected in series (PS mode) can also be used. The equivalent circuit for that in Fig. 2(a) is also simple, as shown in Fig. 2(b). Here

r_1 is the primary winding resistance, jx_1 is the primary leakage inductance, $-jxc_1$ is the primary capacitance, r_2 is the secondary winding resistance, jx_2 is the secondary leakage inductance, $-jxc_2$ is the secondary capacitance, r_c is the core loss, jx_L is the mutual inductance, and R_L is the load resistance.

When C_2 is connected, the following equation holds for a resonance frequency ω_0

$$x_{c2} = \frac{1}{\omega_0 c_2} = x_L + x_2 \quad (1)$$

The overall impedance for the circuit in the absence of c_1

$$Z = \left(\frac{x_L}{x_L + x_2} \right)^2 R_L + j \left(\frac{x_L x_1 + x_1 x_2 + x_2 x_L}{x_L + x_2} \right) \quad (2)$$

When c_1 is connected, the condition for which the imaginary part of Z becomes zero is given by

$$x_{c1} = \frac{1}{\omega_0 c_1} \quad (3)$$

For the equivalent circuit shown in fig(b), the transmission efficiency considering the copper and core losses is as follows

$$\eta = \frac{R_L I_L^2}{R_L I_L^2 + r_c I_0^2 + r_1 I_1^2 + r_2 I_2^2} \quad (4)$$

$$I_0 = I_1 + I_2 \quad (5.2)$$

When the turn's ratio of the two coils is 1:1, the relationships between Currents can be expressed as

$$I_1 = \alpha I_L, \quad \alpha = \frac{x_L + x_2}{x_L} \quad (5.1)$$

$$|I_2| = |I_L| \sqrt{1 + \left(\frac{R_L}{x_{c2}} \right)^2} \quad (5.3)$$

$$|I_0|^2 = I_L^2 \left[\alpha^2 + 1 + \left(\frac{R_L}{x_{c2}} \right)^2 \cos \phi \right], \quad \cos \phi = \frac{x_{c2}}{\sqrt{R_L^2 + x_{c2}^2}} \quad (5.4)$$

Substituting eqn (5) into eqn (4)

$$\eta = \frac{R_L}{R_L + r_1 \alpha^2 + r_2 \left\{ 1 + \left(\frac{R_L}{x_{c2}} \right)^2 \right\} + r_c \left\{ \alpha^2 + 1 + \left(\frac{R_L}{x_{c2}} \right)^2 - 2\alpha \sqrt{1 + \left(\frac{R_L}{x_{c2}} \right)^2} \cos \phi \right\}} \quad (6)$$

Where,

$$R_L = x_{c2} \sqrt{\alpha^2 \frac{r_1}{r_2} + 1} \quad (7)$$

Thus, the maximum transmission efficiency considering the copper and core losses is [6]

$$\eta_{max} = \frac{1}{1 + \frac{2r_2}{x_{c2}} \sqrt{\alpha^2 \frac{r_1}{r_2} + 1} + \frac{r_c \left(\alpha^2 \left(1 + \frac{r_1}{r_2} \right) - 2\alpha \sqrt{\alpha^2 \frac{r_1}{r_2} + 2 \cos \phi + 2} \right)}{x_{c2} \sqrt{\alpha^2 \frac{r_1}{r_2} + 1}}} \quad (8)$$

Here, k and the quality factors for the two coils (Q_1 & Q_2) Q_1 are defined as follows

$$Q_1 = \frac{\omega_o L_1}{r_1}, Q_2 = \frac{\omega_o L_2}{r_2}, k = \frac{M}{\sqrt{L_1 L_2}}, M = \frac{x_L}{x_L + x_2} L_2 \quad (9)$$

Since eqn (10) is true under any conditions, the maximum efficiency can be approximated as shown by eqn(11)

$$\frac{1}{k^2} \frac{Q_2}{Q_1} > 1 \quad (10)$$

$$\eta_{max} \approx \frac{1}{1 + \frac{2}{k\sqrt{Q_1 Q_2}} + \frac{2r_c(k+k^{-1}-1)}{r_2 Q_2}} \quad (11)$$

Three conclusions can be derived from (12): 1) a large value of the product of k and Q yields high efficiency, 2) a large value of the product of r_2 and Q_2 (i.e., ωL_2) is also required for high efficiency, and 3) both copper and core losses increase with decreasing k (i.e., increasing transmission distance). It was not necessary to consider core loss for a high-frequency system without a magnetic core.

4 MATLAB SIMULATION

Simulation for the above circuit diagram is done by using the mat lab Simulink tools and input and output wave forms are shown below.

Mat Lab Simulation for Resistive load

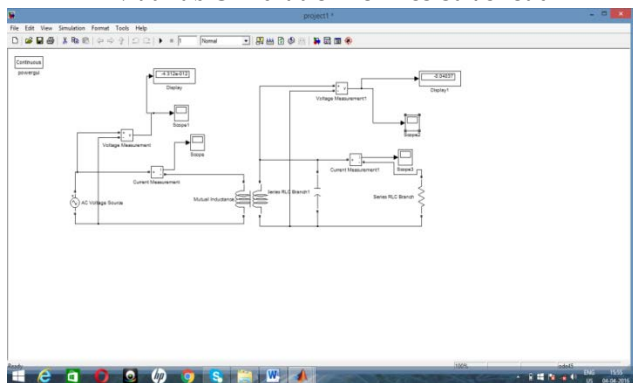


Fig (3):- Simulation circuit for resistive load

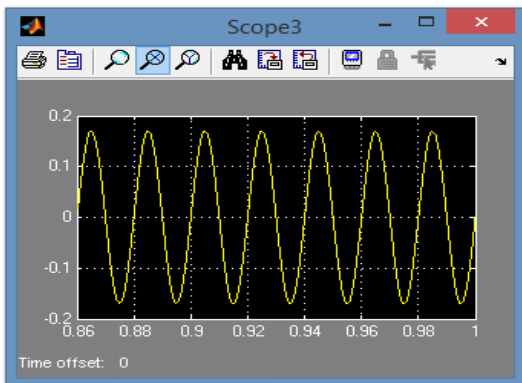


Fig (4):-Output current

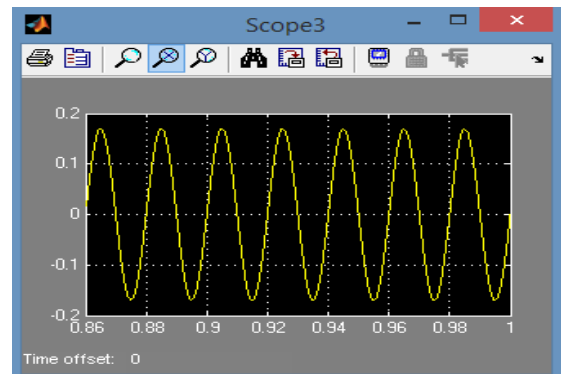


Fig (5):-Output Voltage Mat Lab Simulation for Multi load

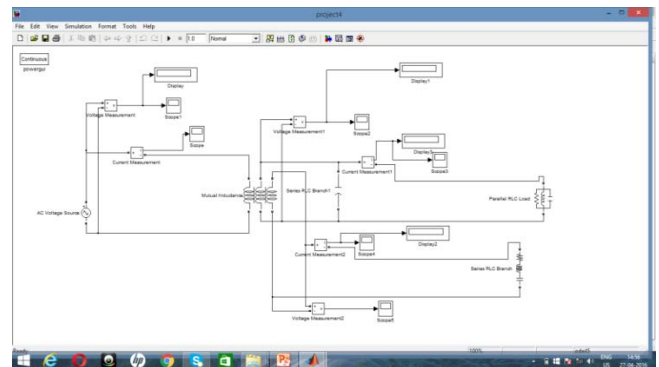


Fig (6):- Simulation circuit for Multi load

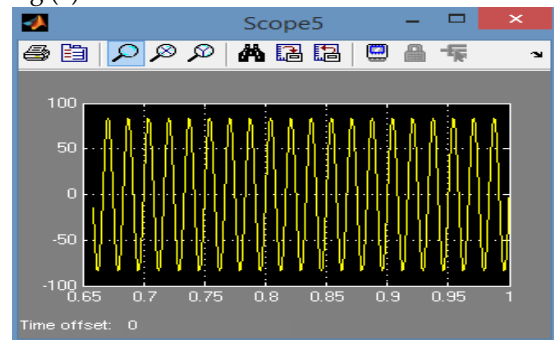


Fig (7):- Output Voltage for load 1

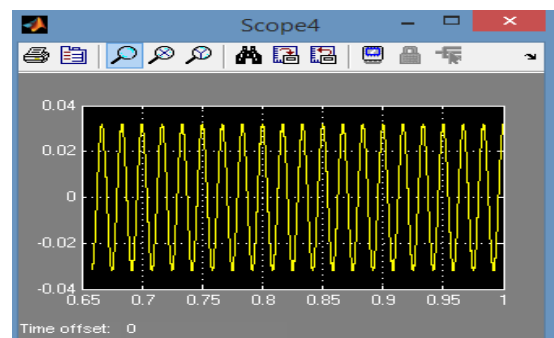


Fig (8):- Output current for load 1

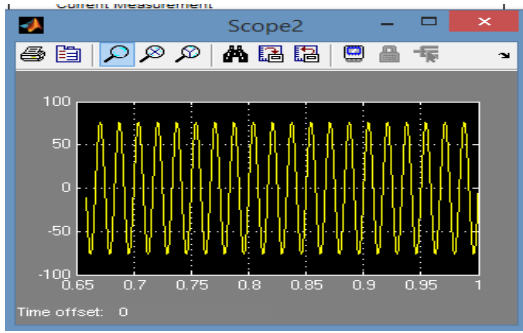
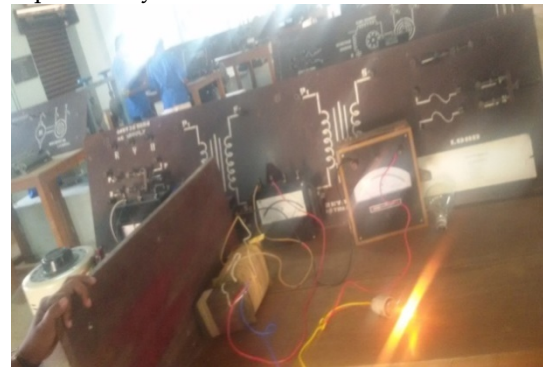


Fig (9):-Output voltage for load 2



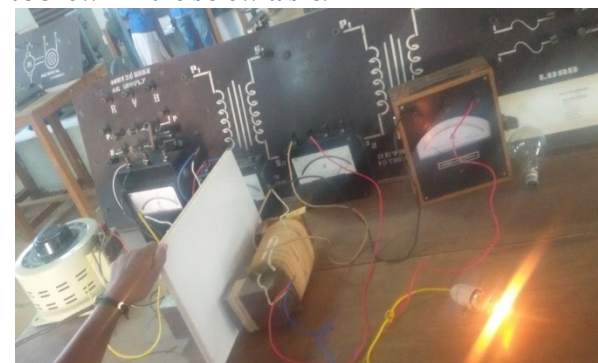
EXPERIMENTAL SET UP FOR WTP IN WOOD MEDIUM

Experimental set up for wireless power transfer is as shown in figure. Here the transmitter and receiver are separated by a 2cm distance



EXPERIMENTAL SETUP FOR WTP IN CONCRETE MEDIUM

The experimental setup of concrete medium is as shown in fig. Here a concrete of thickness 2cm is placed between Transmitter and Receiver. Obtained values are tabulated as shown in the below table.



6 FFT ANALYSIS

The total harmonic distortion obtained for one of the signal of wireless power transfer for resistive load is as shown in the fig(12)

Distance in cm	I/p V ₁ in Volvo	I/p I ₁ in Amps	O/p V ₂ in volts	O/p I ₂ in Amps
4	180	5	74	0.25
6	180	5	70	0.24
10	180	5	36	0.22
12	180	5	32	0.2

5 EXPERIMENTAL SETUP

Experimental set up for air medium

Experimental set up for wireless powertransfer is as shown in figure. Here the transmitter and receiver are

Distance in cm	I/p V ₁ in Volvo	I/p I ₁ in Amps	O/p V ₂ in volts	O/p I ₂ in Amps
4	180	5	74	0.25
6	180	5	70	0.24
10	180	5	36	0.22
12	180	5	32	0.2

separated at respective distances and obtained values are tabulated as shown in the below table, as the distance increases the output voltage get decreases.

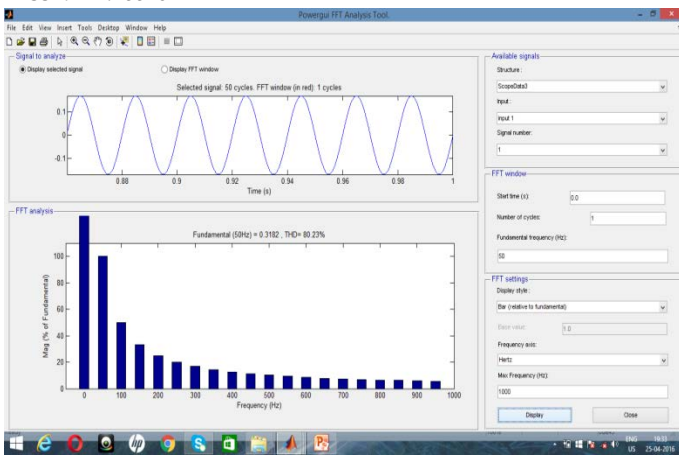


Fig (13):- FFT analysis of output voltage, THD of 80.23

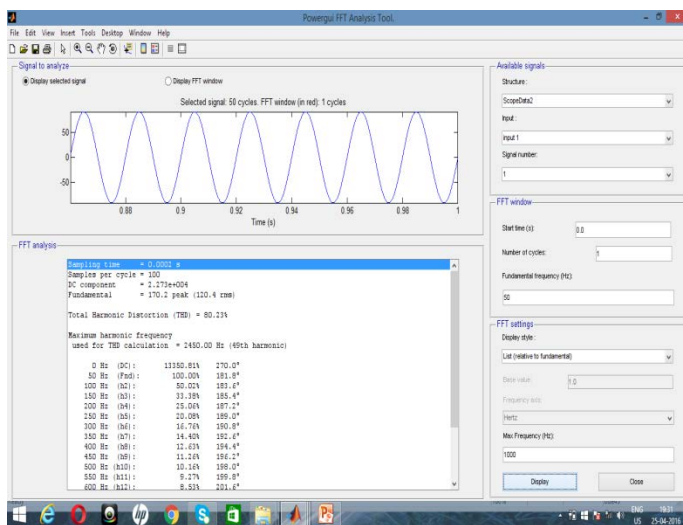


Fig (14):- FFT analysis of output current, THD of 80.23

7 CONCLUSION

Obtaining a large Q factor is difficult at low frequencies, which is the reason why low-frequency approaches have not been used until now. However, when silicon steel is used as the magnetic core

The efficiency depends upon the shape of magnetic pole pieces, here the rectangular shape pole piece are used.

To achieve still more efficiency we can go for single and double flare shape of pole pieces.

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